

$$1. a) \quad t_{\text{settle}} = \frac{2}{\pi} \frac{\Sigma}{\Omega_k \rho_d a} e^{-2z^2/h^2}$$

(eq. 110)

also can use eq. 116

Then integrate to get  $t_{\text{settle}}$

Use  $2a \approx h$

For  $a \sim 10 \text{ cm}$

$$t_{\text{settle}} \sim 3 \text{ yr}$$

b) Epstein & Re < 1 Stokes regime make sure

$$\eta \sim \frac{\rho_s a^2}{2\eta_k}$$

Using  $n \sim 3$

$$\frac{h}{r} \sim \frac{G_s}{v_k} \sim 0.05 \quad \eta \sim 0.008$$

$$\frac{v_r}{v_k} \sim \frac{-\eta}{r + r^{-1}} \quad (128)$$

For 10 cm  $C \sim 1$  maximal drift speed

$$v_r = -\frac{\eta}{2} v_k \sim 100 \text{ m/s}$$

timescale for drifting to the star  $t_d \sim 50 \text{ yr}$

[Note: depending on what you assume in the values it can be few 10s to 100 yr].

c)

$$\text{Reynolds number } Re = \frac{2a v_k}{\Delta C_s} \quad [(102) \& (72)]$$

$$\text{For } 6 \text{ km} \quad Re \sim \frac{2a \eta^{1/2} v_k}{\Delta C_s} \quad \eta \sim 10^{-5}$$

$$\sim \text{large } > 800$$

$$G = 0.44$$

List of typical properties  
at 1 AU

$$\Sigma \approx 10^3 \text{ g cm}^{-2}$$

$$\rho_d \sim 3 \text{ g cm}^{-3}$$

$$\rho_s \sim 5 \times 10^{-10} \text{ g cm}^{-3}$$

off midplane

$$a \sim 1 \text{ cm}$$

$$G_s \sim 1.5 \times 10^5 \text{ cm s}^{-1}$$

$$F_D = -\frac{1}{2} C_D \pi a^2 \rho v^2$$

$$= -\frac{1}{2} \cdot 0.44 \cdot \pi \cdot (8 \text{ km})^2 \cdot (5 \text{e}^{-10}) \cdot \eta v_k^2$$

~ You can thus calculate  $t_{\text{fric}}$  using

$$t_{\text{fric}} = \frac{mv}{|F_D|} \quad (104)$$

I will simply use eq. (105) to avoid doing all of this myself.

[Note: All this is necessary since (105) is not valid in this size range.]

$$t_{\text{fric}} = \frac{mv}{|F_D|}$$

$$= \frac{4}{3} \pi a^3 \rho_d$$

$$\frac{1}{2} C_D \pi a^2 \rho v^2$$

$$= \frac{8}{3} \frac{1}{C_D} \frac{\rho_d}{\rho} \frac{a}{v}$$

$$r = \sqrt{2} t_{\text{fric}} = \gamma v_k \cdot t_{\text{fric}}$$

$$= \gamma v_k \cdot \frac{8}{3} \frac{1}{C_D} \frac{\rho_d}{\rho} \frac{a}{\eta^{1/2} v_k}$$

$$= \frac{8}{3 C_D} \cdot \frac{\rho_d}{\rho} \cdot \frac{a r}{\eta^{1/2}}$$

Check values  
may not be correct  
The method & equations  
should be correct.

Putting values

$$\rho_d = 3 \text{ g cm}^{-3}$$

$$\rho = 5 \text{e}^{-10} \text{ g cm}^{-3}$$

$$C_D = 0.44$$

$$a = 8 \text{ km}$$

$$\gamma = 1 \text{ AU}$$

$$\eta \sim 2 \text{e}^5$$

$$r \sim 10^{27}$$

$$v_r \sim v_k \cdot 10^{-22}$$

$$t_{d, 8 \text{ km}} \sim 10^{21} \text{ yr}$$

d) This happens on a free fall timescale

$$t_{ff} = \sqrt{\frac{\lambda_{crit}^3}{2Gm}}$$

$$= \sqrt{\frac{4G^3 \Sigma^3}{2G^4 \Sigma^3 m}}$$

$$\lambda_{crit} = \frac{2c_s^2}{G\Sigma_{solid}}$$

$$\sim 3 \times 10^{16} \text{ cm.}$$

Using  $\Sigma \sim 10^3 \text{ g cm}^{-2}$ ,  $c_s \sim 10^5 \text{ cm s}^{-1}$ ,  $m \sim 10^{18} \text{ g}$   
 $\Sigma_{solid} \sim 10 \text{ g cm}^{-2}$

$t_{ff} \sim 1 \text{ hour.}$

d) 
$$a = \frac{\sigma \Omega}{\pi G \Sigma}$$

For this use  $\Sigma = \Sigma_{dust} \sim 10^{-2} \Sigma \sim 10 \text{ g cm}^{-2}$

Setting  $a = 1$  you get  $\sigma = 10 \text{ cm s}^{-1}$

$$\lambda_{crit} \equiv \text{KW most unstable wavelength} = \frac{2\sigma^2}{G\Sigma_{dust}}$$

$$\approx 3 \times 10^8 \text{ cm.}$$

$$m \sim \frac{4}{3} \pi \Sigma_{dust} \lambda_{crit}^2 \sim 3 \times 10^{18} \text{ g.}$$

$$t_{ff} = \sqrt{\frac{\lambda_{crit}^3}{2Gm}} = 0.3 \text{ yr.}$$

$$e) \quad t_{\text{type II}} \sim \frac{2}{3\alpha} \left( \frac{h}{r} \right)^{-2} \Omega^{-1}$$

$$\approx 4 \times 10^3 \text{ yr.}$$

$$\alpha \sim 10^{-2}$$

$$\frac{h}{r} \sim 0.05$$

$$\Omega_{100} \sim 2 \times 10^{-7} \text{ s}^{-1}$$

f) ~~the~~ This is growth by core accretion

$$\frac{dM}{dt} = \frac{1}{2} \Sigma_p \Omega \pi R_s^2 F_g$$

Assume  $F_g = 10$ .

$$M = \frac{4}{3} \pi \rho_d R_s^3$$

$$dM = \frac{4}{3} \pi \rho_d \cdot 3 R_s^2 dR_s = 4 \pi \rho_d R_s^2 dR_s$$

$$\cancel{4 \pi \rho_d R_s^2} \frac{dR_s}{dt} = \frac{1}{2} \Sigma_p \Omega \pi R_s^2 F_g$$

$$\frac{dR_s}{dt} = \frac{1}{8} \frac{\Sigma_p \Omega F_g}{\rho_d}$$

$1 M_\oplus$  equivalent to  
 $1 R_\oplus$

$$\int dR_s = \frac{\Sigma_p \Omega F_g}{8 \rho_d} \int dt$$

$$\tau_{\text{form}, 1M_\oplus} \sim \frac{8 \rho_d}{\Sigma_p \Omega F_g} \cdot R_\oplus \sim 24 \times 10^6 \text{ yr.}$$

Note! This is long. Indicates  $F_g$  must be very high  $\sim 10^3$  or higher.

g) For  $10 M_\oplus$  with  $F_g = 10$ .  $10 M_\oplus \sim 10^{1/3} R_\oplus$

$$\tau_{\text{form}, 10M_\oplus} \sim 10^{1/3} \tau_{\text{form}, 1M_\oplus} \sim 52 \text{ Myr.}$$

h) ~~part~~ For SS disk  $\alpha \sim 10^{-2}$  &  $\left(\frac{h}{r}\right) \sim 0.05$

Viscous timescale

$$\tau \sim \left(\frac{h}{\delta}\right)^{-2} \frac{1}{\alpha \Omega} \sim 1 \text{ Myr}$$

i) 100 Myr (given)

h)  $10^6 - 10^7$  yr.

2. a) No.

There is no gravity. Convection needs buoyancy forces.

Diffusion will work since it just depends on the random

thermal motion of molecules.

b). Hydrostatic equilibrium

$$dP = -g \rho dz'$$

$$\frac{dP}{dz'} = -g \frac{\rho M_a m_{amu}}{kT}$$

$$P = NkT$$

$$= \frac{\rho kT}{M_a m_{amu}}$$

$$\frac{dP}{P} = -g \frac{M_a m_{amu}}{kT} dz'$$

$$P = P(0) \exp \left\{ - \int_0^z dz' / H_p(z') \right\} \quad \text{where, } H_p(z) = \frac{kT}{g M_a m_{amu}}$$

Similarly, by replacing  $P$  by  $S$  you will find

$$H_g(z) = \left[ \frac{1}{T(z)} \cdot \frac{dT}{dz} + \frac{g M_a m_{amu}}{kT} \right]^{-1}$$

c) If in a region  $\frac{dT}{dz} = 0$ ,  $H_p = H_g$ .

3. Remember from simple thermodynamics we derived

(a)

good idea to make sure you understand how this is derived (in class)

From hydrostatic equilibrium,  $\frac{1}{\rho} \frac{dP}{dz} = -g$  (2)

For dry case,  $C_p dT = \frac{1}{\rho} dP - L_3 dw_3$   
 $\Rightarrow \frac{dP}{dT} = \rho [C_p + L_3 \frac{dw_3}{dT}]$  (1)

Using (1)  $\frac{dT}{dP} = \frac{dT}{dz} \cdot \frac{dz}{dP} = - \frac{dT}{dz} \cdot \frac{1}{\rho g}$  using (2)

Using (1)

$$\frac{dT}{dP} = \frac{1}{\rho [C_p + L_3 \frac{dw_3}{dT}]} = - \frac{dT}{dz} \cdot \frac{1}{\rho g}$$

$$\frac{dT}{dz} = - \frac{g}{C_p + L_3 \frac{dw_3}{dT}}$$

b)  $\frac{dT}{dz} \approx 10 \text{ K km}^{-1} = - \frac{g}{C_p}$

$C_p \approx \frac{g}{dT/dz} \approx \frac{10 \text{ m/s}^2}{10 \times 10^{-3} \text{ K/m}} \approx 10^3 \text{ erg/K/g}$

$\approx \frac{10 \times 10^2 \text{ (cm s}^{-2}\text{)}}{10 \times 10^{-5}} \approx 10^7 \text{ erg/K/g}$

dPL(b)

Saturation vapor pressure

$P = P_0 e^{-\frac{g z}{R_{\text{gas}} T}}$

$= 2 \times 10^7 \text{ (bar)}$

$e^{-\frac{5.1 \times 10^{11} \text{ erg mole}^{-1}}{280 \text{ K} \cdot 18 \text{ g/mole}}}$

$R_{\text{gas}} \sim \text{erg/g/K}$

$R_g \sim 8.3 \times 10^7 \text{ erg/K/mole}$

$$dP_L(b) P_{sat} = Q e^{-\frac{L_s}{R_g T}}$$

$$R_g = 8.31 \times 10^7 \text{ erg/k/mole}$$

$$T = 280 \text{ K}$$

$$L_s = 5.1 \times 10^{11} \text{ erg/mole}$$

$$\frac{L_s}{R_g T} = \frac{5.1 \times 10^{11} \text{ erg k/mole}}{8.31 \times 10^7 \cdot 280 \text{ mole} \cdot \text{erg k}}$$

$$\approx 21.92 \quad (\text{make sure this is dimensionless})$$

$$P_{sat} = 3 \times 10^7 \cdot e^{-21.92} \text{ bar} \approx 9 \times 10^{-3} \text{ bar}$$

So the partial vapor pressure  $\sim P_{sat}/p \sim 9 \times 10^{-3}$ .

dPL(c) Mean molecular mass of air assuming 20%  $O_2$  + 80%  $N_2$

$$= \left[ \frac{.2 \times 32}{O_2} + \frac{.8 \times 28}{N_2} \right] \text{ g/mole}$$

$$= 28.8 \text{ g/mole}$$

$$\text{Water} = 18 \text{ g/mole}$$

$$\therefore \omega_g = 9 \times 10^{-3} \cdot \frac{18}{28.8} = 5.6 \times 10^{-3}$$

$$dPL(d) \quad L_s = 5.1 \times 10^{11} \text{ erg/mole} = \frac{5.1 \times 10^{11}}{18} \text{ erg/g} = 2.8 \times 10^{10} \text{ erg/g}$$

$$\frac{dT}{dz} = \frac{g}{Q + L_s \frac{d\omega_g}{dz}} \sim \frac{980}{10^7 + \frac{2.8 \times 10^{10} \times 5.6 \times 10^{-3}}{280}}$$

$$= 9.3 \times 10^{-5} \text{ K/cm}$$

$$= 9.3 \text{ K/km}$$

Note: This will be more complicated if  $g$  is not constant.

c) (i) Done in Sec. 3.3.1 Convince yourself.

~~Yes~~

(ii) From hydrostatic equilibrium

$$\frac{dT}{dz} = -\frac{1}{\rho g} \frac{dP}{dz}$$

4. dPL (3.26)

(a)  $F = \sigma T_{\text{effective}}^4$

$$T_e = \left(\frac{F}{\sigma}\right)^{1/4}$$

$$F = \frac{L_0}{4\pi R^2} (1 - A_b) \quad \text{incident flux}$$

Rapidly rotating means  $T$  variation is low as a function of longitude.

Equilibrium temperature.

$$P_{\text{in}} = (1 - A_b) \frac{L_0}{4\pi R^2}$$

$$P_{\text{out}} = 4\pi R^2 \epsilon \sigma T_{\text{eq}}^4$$

$P_{\text{in}} = P_{\text{out}}$  in equilibrium

$$4\pi R^2 \epsilon \sigma T_{\text{eq}}^4 = (1 - A_b) \frac{L_0}{4\pi R^2}$$

$$T_{\text{eq}} = \left[ \frac{(1 - A_b) L_0}{16\pi \epsilon \sigma R^2} \right]^{1/4}$$



Effective  $T$  is = equilibrium  $T$ .

b) Using 3.78 & 3.79.

$$T_e^4 = 2T_0^4 \quad \Rightarrow T_0 = \left(\frac{1}{2} T_e^4\right)^{\frac{1}{4}} = 0.84 T_e.$$

$$T^4 = T_0^4 \left(1 + \frac{3}{2} \tau\right) \\ = \frac{1}{2} T_e^4 \left(1 + \frac{3}{2} \tau\right).$$

$$T = T_e \quad \text{if } \tau = \frac{2}{3}.$$

$$d) T_g^4 = T_e^4 \left(1 + \frac{3}{4} \tau_g\right) \quad \tau_g = 10 \\ = T_e^4 \left(1 + \frac{30}{4}\right) \\ = 8.5 T_e^4$$

5. a)  $\frac{dT}{dz} = -\frac{g(z)}{g}$

$$g(z) = \frac{GM}{(R+z)^2}$$

$$= \frac{\frac{4}{3} \pi R^3 \rho G}{(R+z)^2}$$

$$= \left(\frac{4}{3} \pi \rho R G\right) \frac{1}{\left(1 + \frac{z}{R}\right)^2}$$

At the top of troposphere (tropopause)

b) For Earth  $\frac{z}{R} \approx 0.003$

$$= C \cdot \left(1 - \frac{2z}{R} + \text{higher order terms}\right)$$

For Titan  $\frac{z}{R} \approx 0.02$

For Earth error  $\approx 0.6\%$

For Titan error  $\approx 4\%$

More important to consider this on Titan.

G. dPL 109.

Asteroid

$$B_{\text{ast}} \propto \frac{1}{r_0^2 r_\Delta^2} \Rightarrow B_{\text{ast}} = C_1 \frac{1}{r_0^2 r_\Delta^2}$$

$$B_{\text{comet}} \propto \frac{1}{r_0^{\xi} r_\Delta^2} \Rightarrow B_{\text{comet}} = C_2 \frac{1}{r_0^{\xi} r_\Delta^2}$$

$$\text{At } r_0 = 3 \text{ AU} \text{ \& } r_\Delta = 2 \text{ AU} \quad B_{\text{ast}} = B_{\text{comet}}$$

( $\xi - 2$ )

$$\frac{B_{\text{ast}}}{B_{\text{comet}}} = \frac{C_1}{C_2} \cdot r_0^{\xi - 2} = 1$$

$$\frac{C_1}{C_2} = r_0^{2 - \xi} = 3^{(2 - \xi)}$$

$$\text{At } r_0 = 2 \text{ AU} \text{ \& } r_\Delta = 2 \text{ AU}$$

$$\begin{aligned} \frac{B_{\text{ast}}}{B_{\text{comet}}} &= \frac{C_1}{C_2} r_0^{(\xi - 2)} = 3^{(2 - \xi)} \cdot 2^{(\xi - 2)} = \left(\frac{2}{3}\right)^{(\xi - 2)} \\ &= \frac{3^2}{2^2} \cdot \left(\frac{2}{3}\right)^{\xi} \\ &= \frac{9}{4} \cdot \left(\frac{2}{3}\right)^{\xi} \end{aligned}$$

If  $\xi = 2$  then they are the same.

for  $\xi > 2$ ,  $B_{\text{ast}} > B_{\text{comet}}$

7. dPL 8.5

$$v_{\infty} = \sqrt{\frac{2g_p m}{G \rho_g A}}$$

$$= \sqrt{\frac{8}{3} g G^{-1} \rho_g^{-1}} \cdot (R \rho_g)^{1/2}$$

$$\frac{2g \cdot \frac{4}{3} \pi R^2 \rho_g}{G \rho_g \cdot \pi R^2}$$

$$= \frac{8}{3} \frac{g R}{G} \left( \frac{\rho_g}{\rho_g} \right)$$

Assume  $\rho_g = 10^{-3} \text{ g cm}^{-3}$ .

Then just put values & get answers for each part.  
Make sure to remember how to derive.

8. dPL 6.2

Pressure exerted by self-gravity. Assume hydrostatic equilibrium either by gravity or by material strength.

$$\frac{dP}{dr} = -g \rho$$

$$dP = - \frac{G M_r}{r^2} \rho dr$$

$$= -G \frac{\frac{4}{3} \pi r^3 \rho}{r^2} \rho dr$$

$$= - \frac{4\pi}{3} G \rho^2 r dr$$

$$\int_{P_c}^0 dP = - \int_0^R \frac{4\pi}{3} G \rho^2 r dr$$

$$P_c = \frac{2\pi}{3} G \rho^2 R^2$$

$$a) P_c = \frac{2\pi}{3} G \rho^2 R^2$$

if  $P_c \geq S_m$  center is compressed.

$$\therefore R_{min,c} = \left[ \frac{3 S_m}{2\pi G \rho^2} \right]^{1/2}$$

$$b) P_{1/2} =$$

$$\frac{1}{2} \frac{4}{3} \pi R^3 \rho = \frac{4}{3} \pi R_{1/2}^3 \rho$$

$$= \frac{2\pi}{3} G \rho^2 R^2 - \frac{2\pi}{3} G \rho^2 R_{1/2}^2$$

$$R_{1/2} = \left( \frac{1}{2} \right)^{1/3} R$$

$$= \frac{2\pi}{3} G \rho^2 R^2 \left[ 1 - \left( \frac{1}{2} \right)^{2/3} \right]$$

$$R_{min,1/2} = \left[ \frac{3 S_m}{2\pi G \rho^2 \left( 1 - \left( \frac{1}{2} \right)^{2/3} \right)} \right]^{1/2}$$

c) Just change values.

d) Change values.